

ECE 2001 MASTER PACKET - NOTES:

CH1

- \vec{E} field is same direction as current
- **Load**: anything that excites the circuit + provides a signal
- Four dependent sources - CCVS, CCCS, VCVS, VCCS
- connect **VOLTAGE** in **SERIES**, **CURRENT** in **PARALLEL**

CH2

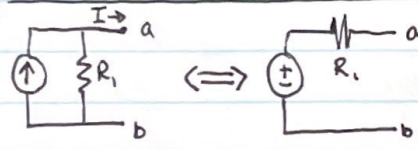
- **essential node**: connection point with 3 or more device
- Kirchoffs Current Law: $\sum I_{node\ out} = 0$
- Kirchoffs Voltage Law: $\sum V_n = 0$
- To **Find Req**: 1) turn off all independent sources
2) apply test current or test voltage
- To **find $V_{Thevenin}$** : leave port open
- To **find I_{Norton}** : Short circuit across ports

CH3

- **Nodal Analysis**: a systematic method used to find the voltage at every essential node in a circuit
- **Mesh Analysis**: method to determine every current in a circuit
- nodes of a grounded end will have a voltage of zero, the other a voltage of the voltage source
- **Floating Voltage Source**: VS where control variable is unknown
↳ add "dummy" variable for missing one
- Nodal analysis works in all circuits, but Mesh only in planar

CH4

Source Transformation Theorem:



□ resistor values are the **SAME**, but the **voltage drops** across them are **NOT**

- $V_{Thevenin}$: equivalent voltage across a circuit
- I_{Norton} : equivalent current across a circuit

$R_{eq} = R_N = R_{TH}$

- **homogeneity // scalability**: $f(\alpha x) = \alpha f(x)$
- **additivity**: $f(x+y) = f(x) + f(y)$
- **Superposition**: the total voltage // current can be found through adding the individual values due to all inputs
↳ **NOT** applicable to power

Superposition steps

- 1) turn off all independent sources, but leave dependent ones untouched
- 2) find desired variable by solving the circuit
- 3) repeat process for all independent sources
- 4) add all results together

$V_{out} = \alpha V_{in} + \beta V_{in}$

only works with linear quantities (WVCR + PWR aren't linear)

Maximum Power Transfer Theorem: at what resistance value is the max pwr absorbed?

$$I_L = \frac{V_{Th}}{R_{Th} + R_{Load}}$$

$$P_L = \frac{V_{Th}^2}{(R_{Th} + R_L)^2} R_L \Rightarrow P_{Lmax} = \frac{V_{Th}^2}{4R_L} \times R_L = R_{Th} \times$$

additional previous equations

$\vec{F}_{electric} = \vec{E}q$	$I(t) = \frac{dQ}{dt}$	$P(t) = \frac{dE}{dt}$ <small>pwr</small>	$P = IV = I^2R = \frac{V^2}{R}$ <small>inst. pwr.</small>
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<u>Conductance</u> : $G = \frac{1}{R}$	$R = \frac{\rho l}{A}$ <small>R = resistance ρ = resistivity l = length A = cross. sec. area</small>	$V = IR$
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CH5

Capacitors + inductors store energy

- ↳ capacitors store energy in Electric field
- ↳ inductors store energy in magnetic field

* Capacitance eqn: $q = CV$
q = charge
V = voltage

Capacitors depend solely on geometry + material properties & does NOT depend on voltage

Current through a capacitor: $i_c(t) = C \frac{dV_c(t)}{dt}$ V is continuous

$$V_c(t) = V_c(t_0) + \frac{1}{C} \int_{t_0}^t i_c(x) dx \Leftrightarrow V_c(t) = V_c(\infty) + [V_c(t_0) - V_c(\infty)] e^{-\frac{1}{RC}(t-t_0)}$$

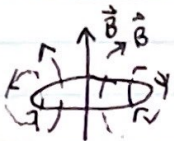
energy stored in capacitor:

$W_{cap} = \frac{1}{2} CV_c^2$	$\gamma = R_{eq} C_{eq}$
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* Inductance eqn:

$$L = \frac{\Phi}{I} = \frac{\mu_0 N^2 S}{l}$$

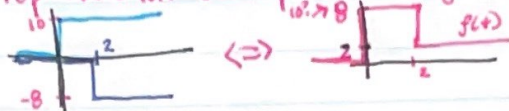
l = length of solenoid
N = # of turns
S = surface area of coil



flux linkage: $\lambda = N\Phi$

* L does NOT depend on current

Step Function example: sketch $f(t) = 10u(t) - 8u(t-a)$



Load Behaviors:

in series:

$R_{eq} = R_1 + R_2$

$\frac{1}{C_{eq}} = \sum_{i=1}^n \frac{1}{C_i}$

$L_{eq} = L_1 + L_2$

in Parallel:

$\frac{1}{R_{eq}} = \sum_{i=1}^n \frac{1}{R_i}$

$C_{eq} = C_1 + C_2$

$\frac{1}{L_{eq}} = \sum_{i=1}^n \frac{1}{L_i}$

* resistors + inductors act alike, + opposit to capacitors behavior! *

CH7 $v(t) = V_m \sin(\omega t + \phi)$

↳ time period T: time it takes for signal to repeat itself

↳ frequency: $f = \frac{1}{T} = \frac{\omega}{2\pi}$

↳ radial frequency: $\omega = 2\pi f$

↳ phase shift ϕ : $v(t)$ will LAG by ϕ degrees

□ the load in a circuit does NOT change the currents wave type

□ in Lin. systems, the output signal will (in steady state)

have the same frequency as the input signal

□ Imaginary number (j): $j = \sqrt{-1}$

□ rectangular form: $X = a + jb$

Polar form: $X = r \angle \theta$
 $r =$ length of magnitude of complex #
 $\theta =$ angle

$X = r \angle \theta = r e^{j\theta}$

□ $|x| = r + \text{angle}(x) = \theta$

Addition + Subtraction - rectangular form

$\left. \begin{matrix} X = a + jb \\ Y = c + jd \end{matrix} \right\} \Rightarrow X - Y = (a - c) + j(b - d)$

Multiplication + Division - polar form

$\left. \begin{matrix} X = r_1 \angle \theta_1 \\ Y = r_2 \angle \theta_2 \end{matrix} \right\} \Rightarrow XY = r_1 r_2 \angle \theta_1 + \theta_2 \quad + \quad \frac{X}{Y} = \frac{r_1}{r_2} \angle \theta_1 - \theta_2$

Taking the reciprocal - Polar Form

$$X = r \angle \theta \Rightarrow \frac{1}{X} = \frac{1}{R} \angle -\theta$$

Squaring or Taking the Square Root - Polar

$$X = r \angle \theta \Rightarrow \begin{cases} \sqrt{X} = \sqrt{r} \angle \frac{\theta}{2} & + & X^{\frac{1}{n}} = r^{\frac{1}{n}} \angle \frac{\theta}{n} \\ X^2 = r^2 \angle 2\theta & + & X^n = r^n \angle n\theta \end{cases}$$

Complex Conjugate - Both Rectangular + Polar

$$X = a + jb = r \angle \theta \Rightarrow X^* = a - jb = r \angle -\theta$$

□ additionally: $j = 1 \angle 90^\circ$ + $\frac{1}{j} = -j = 1 \angle -90^\circ$

□ angle in class will always be $-180 \leq \theta \leq 180$

□ Phasors are NEVER a function of time

* $X(t) = A \cos(\omega t + \phi) \Rightarrow \tilde{X} = A \angle \theta = A e^{j\theta}$ *

↳ $y(t) = B \sin(\omega t + \phi) \Rightarrow B \cos(\omega t + \phi - 90^\circ)$ ← MINUS 90°

□ phasors must be in cosine (-90° if in sine)

□ Euler's Identity: $e^{\pm j\theta} = \cos\theta \pm j\sin\theta$

□ the \sim means phasor representation (\tilde{X})

□ leading is a positive phase shift

lagging is a negative phase shift

□ in the phasor domain, the wave is now a vector with a magnitude equal to the peak value of the wave, + an angle that represents the phase shift of the wave.

□ Kirchhoff's law remains valid in the phasor domain

$$\sum_{n=1}^N \tilde{I}_n = \tilde{I}_1 + \tilde{I}_2 + \dots + \tilde{I}_N = 0 \quad + \quad \sum_{n=1}^N \tilde{V}_n = 0$$

$$\tilde{V}(\omega) = Z(\omega) \tilde{I}(\omega)$$

Impedance (Z): a complex number (NOT a phasor) that is equal to the ratio of the phasor voltage over the phasor current of an element

↳ impedance is only defined for AC signals + measured in (Ω)'s

- in general, impedance is a function of frequency
- Impedance accounts for resistance + reactants effects

□ **Admittance (Y):** $Y = \frac{1}{Z}$ [Similar to how conductance, G , is the inverse of resistance]

units: Siemens

↳ Admittance is NOT a phasor, but a complex number

RESISTORS:

$$\square \frac{V(t)}{R} = i(t) = \frac{1}{R} V_m \cos(\omega t + \theta)$$

- the impedance of a resistor is equal to its resistance

$$\tilde{V}(\omega) = V_m \angle \theta \quad \tilde{I}(\omega) = \frac{1}{R} V_m \angle \theta \quad Y = \frac{1}{Z} = \frac{1}{R} = G$$

- the voltage drop across a resistor is always in phase with the current through it

CAPACITORS:

$$i_c(t) = C \frac{dV_c(t)}{dt} = C \frac{d}{dt} (V_m \cos(\omega t + \theta))$$

$$\Rightarrow i(t) = -\omega C V_m \cos(\omega t + \theta - 90^\circ)$$

$$\tilde{I}(\omega) = \underbrace{j\omega C}_{a} \underbrace{V_m \angle \theta}_{b} \Rightarrow \tilde{I}(\omega) = j\omega C \tilde{V}(\omega) \quad \tilde{V}(\omega) = \tilde{I}(\omega) Z$$

□ **Impedance of a capacitor:** $Z = \frac{1}{j\omega C} = \frac{-j}{\omega C}$ admittance: $Y = \frac{1}{Z} = j\omega C$

- Current (I) LEADS the voltage by 90°
- Voltage (V) LAGS the current by 90°

INDUCTORS:

$$v_L(t) = L \frac{di_L(t)}{dt} = -\omega I_m L \sin(\omega t + \theta^\circ)$$

$$\Rightarrow v(t) = -\omega L I_m \cos(\omega t + \theta^\circ - 90^\circ)$$

$$\tilde{v}(\omega) = \underbrace{j\omega L}_a \underbrace{I_m \angle \theta^\circ}_b$$

$$\tilde{v}(\omega) = j\omega L \tilde{I}(\omega) = \tilde{I}(\omega) Z$$

Impedance of an Inductor:

$$Z = j\omega L$$

admittance:

$$Y = \frac{1}{Z} = \frac{1}{j\omega L}$$

Current LAGS the Voltage by 90° or
Voltage LEADS the current by 90°

THE GENERAL LOAD:

$$v(t) = V_m \cos(\omega t + \theta_v) \quad + \quad i(t) = I_m \cos(\omega t + \theta_i)$$

$$Z_{\text{Load}} = (V_m \angle \theta_v) / (I_m \angle \theta_i)$$

↳ the angle of impedance is equal to the phase difference between the voltage + current

$$Z_{\text{Load}} = R + jX$$

↑ real part: resistance

← imaginary part: reactance

Impedance (Z) acts as a resistor + capacitor

Admittance (Y) acts as an inductor

CH8

capacitors favor HIGH freq, impede LOW freq

inductors favor LOW freq, impede HIGH freq

favor - short circuit
impede - open circuit

we only add phasors in the same frequency,
signals with different frequencies solved in time domain

Average Power:

$$P = \frac{V_m I_m}{2} \cos(\theta_v - \theta_i)$$

recall average: $x = \frac{1}{T} \int_{t_0}^{T+t_0} x(t) dt$

inductors + capacitors do NOT consume power

Instantaneous Power Equation (phasor)

$$P(t) = \frac{V_m I_m}{2} \cos(2\omega t + \theta_v + \theta_i) + \frac{V_m I_m}{2} \cos(\theta_v - \theta_i)$$

The effective value for a periodic signal $x(t)$ can be calculated by taking its Root Mean Square

$$X_{eff} = X_{rms} = \sqrt{\frac{1}{T} \int_{t_0}^{t_0+T} x^2(t) dt}$$

theoretically $P = V_{rms} I_{rms} \cos(\theta_v - \theta_i)$

for maximum power efficiency:

$$Z_{Load} = Z_{eq}^*$$

* = conjugate

Power Efficiency:

$$\eta = \frac{P_{Load}}{P_{Source}}$$

max PWR

$$\omega = 2\pi f$$

Impedance is minimized when $X_L = X_C$

Resonance Frequency: the frequency when the total impedance in the circuit is a minimum, or, the total current is a maximum

$$f_{res} = \frac{1}{2\pi\sqrt{LC}}$$

Shorthand:

$$V_{rms} = \frac{V_{max}}{\sqrt{2}} \quad I_{rms} = \frac{I_{max}}{\sqrt{2}} \quad P = \frac{1}{2} RE \{ \vec{V} \vec{I} \}$$

$$P_{Load, Max} = \frac{|V_{th}|^2}{8R_{eq}} = \frac{|V_{th,rms}|^2}{4R_{eq}}$$

CHA

mutual inductance:

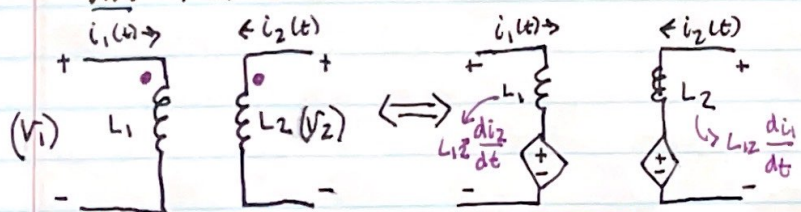
$$L_{12} = \frac{N_2 \Phi_{12}}{I_1}$$

L_{11} = self inductance

$L_{11} > L_{12}$ ALWAYS

$$\Phi_{11} > \Phi_{12} \quad L_{12} = L_{21}$$

- Polarity of induced voltage depends on direction of windings
- The current entering the dotted terminal of one inductor introduces a positive voltage oriented towards the dotted terminal of the other inductor



V_1 is the SUM of both the induced voltage by the current $i_1(t)$ [self inductance] + the voltage induced by the current i_2 going through L_2 [mutual inductance]

Passive Sign Convention:

$$V_1(t) = L_1 \frac{di_1(t)}{dt} + L_{12} \frac{di_2(t)}{dt} \quad + \quad V_2(t) = L_2 \frac{di_2(t)}{dt} + L_{12} \frac{di_1(t)}{dt}$$

the polarity of the dependent source will follow the dot
 ↳ if the dot is at the top of inductor, + sign on V. source is @ top

the sign of the induced voltage will depend on whether the current enters or leaves the dot

↳ if I enters dot, $V_{induced}$ is POSITIVE
 ↳ if I leaves dot, $V_{induced}$ is NEGATIVE } I + v are separate

mesh analysis is often the best solution method

Pinstantaneous between $i_1 + i_2$

↳ $P = V_1(t)i_1(t) + V_2(t)i_2(t)$

$$P = i_1(t)L_{12} \frac{di_2(t)}{dt} + i_2(t)L_2 \frac{di_2(t)}{dt}$$

$W_L = \frac{1}{2} Li^2$ add if same dot convention, subtract if opp.

coupling coefficient: $0 \leq k \leq 1$

$$k = \frac{L_{12}}{\sqrt{L_1 L_2}}$$

for non neg energy: $L_{12} \leq \sqrt{L_1 L_2}$

(self) inductance:

$$\Phi = \int_S \vec{B} \cdot d\vec{s}$$

↳ surface area

$$L = \frac{\Phi}{I}$$

mutual inductance:

$$\Phi_{12} = \int_S \vec{B}_1 \cdot d\vec{s}_2 < \Phi_{11}$$

"flux through 2 due to 1"

mutual inductance

$$L_{12} = \frac{N_2 \Phi_{12}}{I_1} = \frac{\lambda}{I}$$

$L_{11} > L_{21}$
 $L_{12} = L_{21}$

$$L = \frac{\Phi_{11} N_1}{I_1}$$

self inductance

$$\frac{V_2(t)}{V_1(t)} = \frac{N_2}{N_1} = n$$

← N = number of turns
 IDEAL TRANSFORMER

$$\frac{i_2(t)}{i_1(t)} = \frac{-N_1}{N_2} = -\frac{1}{n}$$

no power lost in ideal transformer

ideal transformer has coupling coefficient (k) = 1

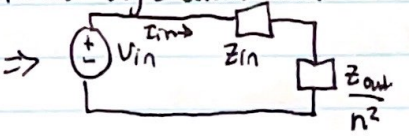
both primary + secondary have same flux

transformers are AC-AC converters, Buck converters are DC-DC

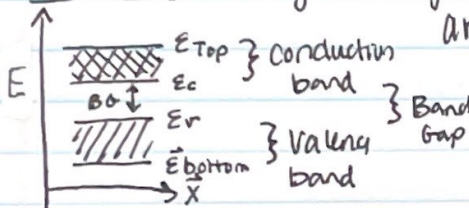
impedance as seen by V_{in} is affected by Z second coil

↳ Reflected Impedance:

$$\frac{Z_{out}}{n^2}$$

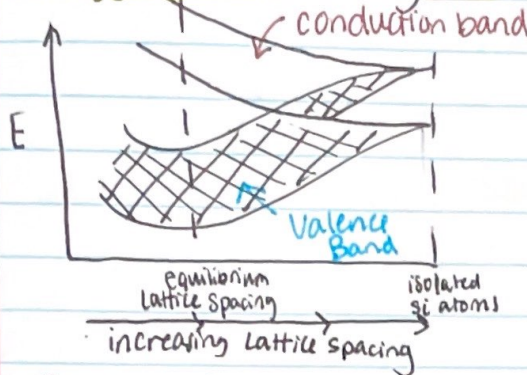


- CH10**
- electron energy levels increase the further orbitals you travel
 - **Aufbau Principle**: the lowest energy orbitals are filled first
 - **Pauli Exclusion Principle**: there is a max of 2 electrons per orbital + opposite spin
 - **Hund's Rule**: equal energy orbitals are filled with 1 electron each in parallel spins before any get a second electron of opp. spin
 - **Ionic Bond**: taking an electron from another atom + the resulting ions are held together by electrostatic attraction of opp. charged. ptcs.
 - **Constructing band** - made up of **anti-bonding orbitals**
valence band - the band of **bonding molecular orbitals**
 - molecular orbital energies in silicon crystals are dependent on bond length
 - ↳ less spacing + bond length, more interactions
 - **Band Gap**: range of energies that electrons within the crystals are unable to obtain



- the **LOWER** the temp, **valence band filled, conduction band empty**
 - ↳ no electrons in conduction band + cannot carry current from lack of excited electrons in valence band
- "Excited" electron requires **Energy \geq band gap**
 - ↳ it is NOT a "free" electron bc it cannot leave the crystal entirely
- **Conduction Band** carries ^{current} from **excited electrons**
Valence Band carries current from **positive holes**
 - ↳ $\uparrow E$ for hole, it moves \downarrow energy band diagram
 - ↳ $\uparrow E$ for electron, it moves \uparrow energy band diagram
- **increase carriers, increase conductivity** (+ vice versa)
- concentration of carriers depends on the Energy required for an electron to jump from valence band \rightarrow conduction band
 - ↳ * **SMALLER BAND GAP \Rightarrow HIGHER CONDUCTIVITY** *
- Conductors like metals have overlapping energy bands + have no band gap

Energy Focused Bonding Model:



□ intrinsic semi-conductor:

extremely pure semi-conductor

↳ impur atoms negligible

□ CARRIER electricity:

electrons traveling due to energy

given that breaks bonds

□ Electron Carrier: when electrons jump along "holes" from electron(s) that broke off

□ Carriers in semiconductors: electrons (-) + holes (+)

□ Carriers in Pure (intrinsic) Semi-conductor

$$n = p = n_i$$

n = free electron concentration
 p = n^+ concentration
 n_i : intrinsic concentration

□ Doping: intentionally introducing impurities to add or remove electrons

↳ donors: give electrons; acceptors: take electrons

□ "n type semi-conductors": $n > p$ (donor doped)

"p type semi-conductors": $n < p$ (acceptor doped)

↳ the larger value, p or n , is majority carrier, + the smaller is the minority carrier

□ Recombination: when e^- + hole encounter + cancel out, releasing \bar{E}

□ Generation: when e^- absorbs \bar{E} , producing e^- /hole pair

□ @ equilibrium, the rates of recombination + generation are =

$$np = n_i^2$$

□ diffusion: the evenness of the carrier concentration with

$$\vec{J} = -D \frac{dn}{dx}$$

respect to position
 \vec{J} : particle flux density; D : proportionality constant; $\frac{dn}{dx}$: particle concentration derivative

$$\vec{F}_{electric} = -q \vec{E} + v_{drift}$$

$$J_{NDrift} = q \mu_n n E_x \quad J_{PDrift} = q \mu_p p E_x \quad J = J_n + J_p$$

J : drift current density
 n : electron concentration
 μ_n : electron mobility
 ← total current density

Einstein Relation:

electrons: $\frac{P_n}{u_n} = \frac{KT}{q}$

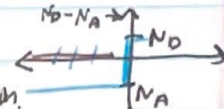
holes: $\frac{D_p}{M_p} = \frac{KT}{q}$

T = temp (Kelvin)
 K = constant
 $\frac{KT}{q}$ @ room temp = 0.0259V

[CH1]

a PN junction is necessary whenever a semi-conductor transitions from a p-type to an n-type

Doping Profile: the difference between the donor concentrations & acceptor concentration.



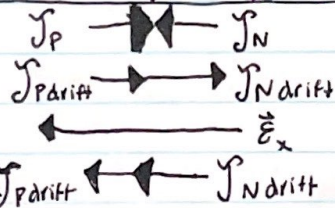
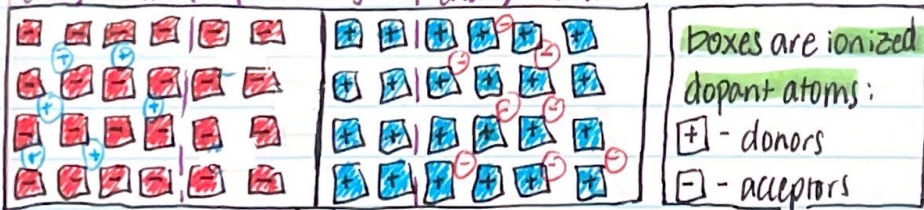
Diffusion: holes diffuse from p-side to n-side while electrons diffuse from n-side to p-side

Depletion Region

- region of reduced majority carrier concentration near the junction, as the majority carriers from each side diffuse across the junction leaving behind fixed ionized dopant atoms & that then results in a charge imbalance
- this charge imbalance creates an \vec{E}_{field} , & creating drift currents that pull e^- back to n side, & holes back to p-side of junction
- As more carriers diffuse across the junction, the drift currents increase with \vec{E}_{field} UNTIL equilibrium is reached

Equilibrium Situation inside a PN Junction:

Charge Neutral | Depletion Region | Charge Neutral

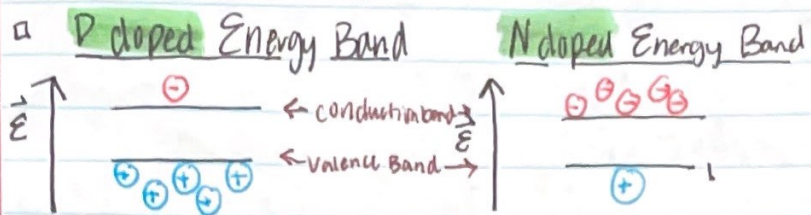


* only majority characters are important

in the depletion region, the total charge concentration is dominated by ionized atoms

$\rho = q(p - n + N_D^+ - N_A^-)$

ρ = total charge density
 $N_D^+ + N_A^-$ = concentration of ionized donor + acceptors



□ increasing the Δ voltage increases band gap width

Rest of Ch 11-13 Not included